

# NUMERICAL IMPLEMENTATION AND CALIBRATION OF A HYSTERETIC MODEL WITH PINCHING FOR THE CYCLIC RESPONSE OF STEEL JOINTS

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**ABSTRACT:** In this paper, a hysteretic model with pinching is presented that is able to reproduce realistically the cyclic response of generic steel joints. Secondly, the computer implementation and adaptation of the model in a spring element within the computer code SeismoStruct is described. The model is subsequently calibrated using a series of experimental test results for steel joints subjected to cyclic loading. Finally, typical parameters for the various joint configurations are proposed.

**Keywords:** structural engineering, steel structures, buildings, component method, beam-to-column joints, dynamic behaviour, seismic behaviour, joint model

## 1. INTRODUCTION

The behaviour of steel or composite joints under cyclic loading is characterized by hysteretic loops with progressive degradation of strength and stiffness that eventually lead to failure of the joint. A typical natural event that, for simplicity, is usually approximated by cyclic loading is an earthquake. Usually, seismic events provoke relatively high amplitudes of rotation in the joint area, so that steel repeatedly reaches the plastic range and the joint fails after a relatively small number of cycles. This typical behaviour is usually called oligocyclic fatigue, in close analogy with the behaviour of steel under repeated cyclic loading stressed into the plastic range (Fig. 1a).

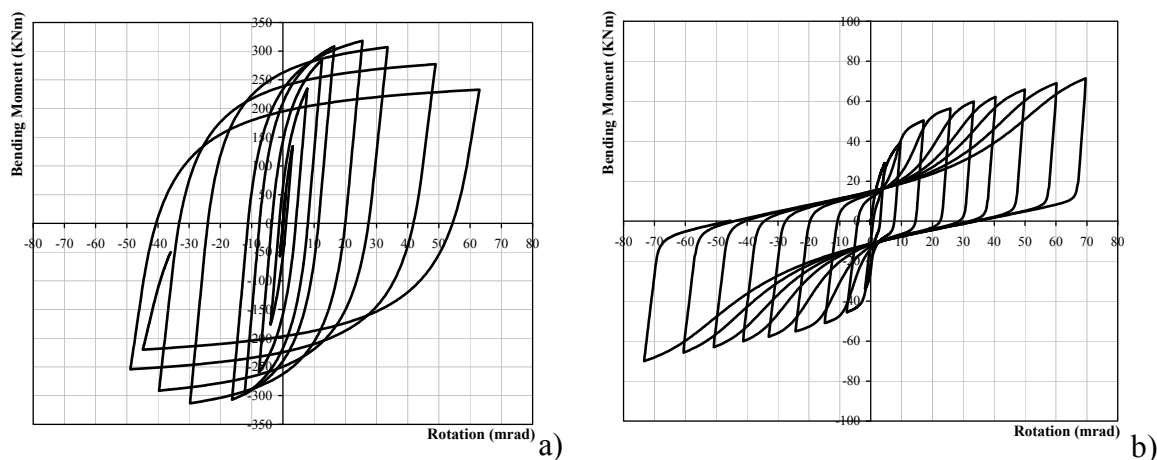


Figure 1. The Loading Branch: a) Without Pinching and b) With Pinching.

Predicting the behaviour of steel and composite joints is quite complex, because it combines several phenomena such as material non-linearity (plasticity, strain-hardening), non-linear contact and slip, geometrical non-linearity (local instability), residual stress conditions and complicated geometrical configurations. Under cyclic loading, this behaviour is further complicated by successive static loading and unloading, as illustrated in Fig. 1b, where the characteristic pinching effect in the loading branches is clearly visible. For static monotonic situations it is nowadays possible to accurately predict the moment-rotation response of a fairly wide range of joint configurations by applying the principles of the component method (Eurocode 3 [18]; Jaspert [21]). However, this is not the case for the cyclic situation. In this case, the usual approach is to develop multi-parameter mathematical expressions that are able to reproduce the range of hysteretic behaviours for a given group of steel joint typologies. Subsequently, the values of the parameters are calibrated to satisfactorily correlate to a range of section sizes for a given group of joint typologies.

Historically, two mathematical formulas have provided the basis for most of the models that have been proposed in the literature: Ramberg-Osgood type mathematical expressions (Ramberg and Osgood [38]), that usually express strain (generalized displacement) as a non-linear function of stress (generalized force) and Richard-Abbott type mathematical expressions (Richard and Abbott [39]), that usually relate generalized force (stress) with generalized displacement (strain).

Ramberg-Osgood based mathematical models were first used by Popov and Pinkey [36] to model hysteresis loops of non-slip specimens and later applied to model the skew symmetric moment-rotation hysteretic behaviour of connections made by direct welding of flanges with or without connection plate (Popov and Bertero [35]). Mazzolani [28] developed a comprehensive model based on the Ramberg-Osgood expressions that was able to simulate the pinching effect, later modified by Simões et al. [43] to allow for pinching to start in the unloading zone. It is noted that models based on the Ramberg-Osgood expressions present the disadvantage of expressing strain as a function of stress, which clearly complicates its integration in displacement-based finite element codes (that constitute the majority of the available applications) or the direct application for the calibration and evaluation of test results, almost always carried out under displacement-control once they reach the non-linear stage.

The Richard-Abbott expression was first applied to the cyclic behaviour of joints by De Martino et al. [10]. Unfortunately, that implementation was not able to simulate the pinching effect (Simões et al. [43]). Subsequently, Della Corte et al. [11] proposed a new model, also based on the Richard-Abbott expressions, that was capable of overcoming this limitation and simulate the pinching effect, as well as strength and stiffness deterioration and the hardening effects.

Since the mid 1980's, several research projects on the cyclic behaviour of steel joints were undertaken in various research centres, comprising a total number of 39 research projects and 216 individual experimental tests. These tests are summarized in tables 1 to 5 and comprise steel joints, ranging from welded configurations to end-plate typologies. In general, the objective of these cyclic tests was the study of the seismic performance of the joints, following the observation of failures resulting from the Kobe and Northridge seismic events.

Table 1. Welded Steel Joints

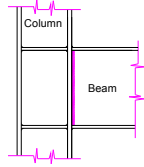
		<p style="text-align: center;">Total number of research projects: 7 Total number of tests: 28 Total number of different load histories: 5</p>		
Authors (date)	N.° of tests	Joint Characterization	Load History	Main parameters investigated
Popov [34]	2	Internal welded joints with beams W460x74 (W18x50) and W610x113(W24x76) column sizes with 13 mm web continuity plates.	(1)	Contribution of the panel zones and column web stiffeners (continuity plates) to joint flexibility in the post-elastic range of behaviour.
Elnashai and Elghazouli [16]	2	One half of two storey frame. Columns in H150x150x7x10, beams in H250x130x9x9 and column web stiffener with 9 mm thickness. One cyclic test and one pseudo-dynamic.	(4)	Investigate the effect of the joints rigidity on the member as well as the frame behaviour. Study the hysteretic joint behaviour.
Elnashai et al. [17]	2	Tests on external two-storey steel frames with rigid joints comprising welded beam (H250x130x9x9) to column (H150x150x7x10).	(4)	Effect of the joint stiffness and capacity on frame response. In addition, a comparison between the behaviour of frames with bolted semi-rigid and fully welded rigid joint is carried out.
Mele et al. [29]	15	Welded beam-to-column joints with beams section IPE300 and columns section HEB160, HEB200 and HEB240 sections and continuity plates 10 mm thick.	(9)	Assessment of the cyclic behaviour, influence of the column size and panel zone design.
Dubina et al. [13]	2	Welded beam (IPE360) to column (HEB300) internal joints	(2)	Initial stiffness, moment capacity and plastic rotation capacity.
Calado [8]	1	Welded steel beam (IPE300) to column (HEB200) external joint.	(2)	Cyclic behaviour, modes of failure.
Grecea et al. [20]	4	Beam-to-column internal welded joints, comprising an H or I column to two cantilever beams, without transverse stiffener in column web.	(2)	Evaluation of cyclic rotation capacity.

Table 2. Welded Flange and Bolted Web Steel Joints

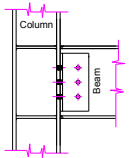
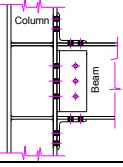
		<p>Total number of research projects: 8            Total number of tests: 38            Total number of different load histories: 6</p>		
Authors (date)	N.º of tests	Joint Characterization	Load History	Main parameters investigated
Popov [34]	5	Internal welded flanges and bolted webs joints. W460x74(W18x50) beams and W610x113(W24x76) columns, with 19 or 13 mm column web continuity plates.	(1)	Contribution of the panel zones and column web stiffeners (continuity plates) to joint flexibility in the post-elastic range of behaviour.
Plumier and Schleich [33]	2	One external joint and one internal joint, combining bare steel elements in section HEB300 and beams in section HEA260.	(2)	Contribution of the shear panel in the energy dissipation. Study the strength and rotation capacity joint.
Tsai et al. [46]	10	External beam to wide flange column joints, using bolted web welded flange. Beams sections W21x50, W21x62, W21x83 and W21x101. All columns W14x159. 8 mm doubler plate welded to the column panel zone in the first test. All specimens have continuity plates of thickness equal to beam flange thickness.	(5)	Quality of beam-flange groove welds, strength of specimens, beam's plastic rotation capacity and effects of web-joint details.
Leon et al. [24, 25]	1	Interior joints, with beam W27x94 and the column W14x211, the panel zone incorporate four continuity plates and doubler plate on both sides of the column web.	(3)	Investigate the modes of failure in the region of the bottom flange, specially the effect of the composite concrete slab.
Lu et al. [27]	4	External joints with the flange beam (W36x150) welded to column (W14x311) and web beam bolted plate.	-	Effect of the weld metal toughness.
Stojadinovic et al. [44]	10	External joints with the flange beam welded to column and web beam bolted plates. W36x150, W30x99, W24x68 beam sizes and W14x120 to W14x257 column sizes.	(10)	Investigate the parameters beam size, panel zone strength and material properties of beam steel.
Yu and Uang [48]	4	External beam (W30x99) to column (W14x176) joints.	(11)	Evaluate the effects of the near-failure loading and extra lateral bracing.
Dubina et al. [13]	2	Welded cover plates and web cleats beam (IPE360) to column (HEB300) internal joints	(2)	Initial stiffness, moment capacity and plastic rotation capacity.

Table 3. Top and Seat Steel Joints



Total number of research projects: 8  
Total number of tests: 53  
Total number of different load histories: 6

Authors (date)	N. <sup>o</sup> of tests	Joint Characterization	Load History	Main parameters investigated
Elnashai and Elghazouli [16]	2	One half of the two storey frame. Columns in H150x150x7x10, beams in H250x130x9x9 and column web stiffener with 9mm thickness. One cyclic test and one pseudo-dynamic.	(4)	Investigate the effect of the semi-rigid joints on the member as well as the frame behaviour. Study the hysteretic joint behaviour.
Bernuzzi et al. [4]	4 + 1	External top and seat angle joints, with beam IPE300 attached to a rigid counterbeam.	(2)	In the first series study the influence of load history. The second series study the influence of the key geometrical and mechanical parameters in the cyclic performance.
Elnashai et al. [17]	5	Tests on two-storey steel frames with semi rigid joints comprising of top, seat and web angles. Beams in H250x130x9x9 and UB 254x146x31 sections and columns in H150x150x7x10 and UC 203x203x6 sections.	(4)	Effect of the joint stiffness and capacity on frame response. In addition, a comparison between the behaviour of frames with bolted semi-rigid and fully welded rigid joint is carried out.
Shen and Astaneh-Asl [42]	6	Bolted-angle beam-to-column joints, with W360x179 column size.	(7)	Inelastic behaviour under large cyclic deformation, failure modes and energy dissipation capacity.
Kukreti and Abolmaali [23]	12	Bolted top and seat angle steel joints with column W200x100 and beam sizes W360x64 and W410x67.	(8)	Approach toward formulating analytical models to predict the moment-rotation hysteresis behaviour, including the initial stiffness, ultimate moment capacity, ultimate rotation.
Abolmaali et al. [1]	20	Double web angle external joints, with the angles bolted in beam and bolted in the column and welded-bolted. W410x67 beam size and W200x100 column size.	(8)	Moment-rotation hysteresis loops and the failure modes.
Calado [8]	1	Bolted top, seat and web angle steel external joint with IPE300 beam size and HEB200 column size.	(2)	Cyclic behaviour, modes of failure.
Leon et al. [26]	2	Top, web and seat angle external joints with W460x60 beam size and W360x216 column size.	(3)	Strength, stiffness and rotation capacity.

Table 4. Bolted End-plate Steel Joints

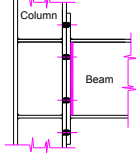
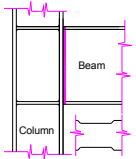
		Total number of research projects: 12 Total number of tests: 87 Total number of different load histories: 3		
Authors (date)	N.º of tests	Joint Characterization	Load History	Main parameters investigated
Korol et al. [22]	7	External extended end plate joints with beam haunch, and with or without transverse web column stiffeners. Beams in W360x45 and W360x57, and columns in W360x64 and W360x79.	-	Seismic performance in terms of strength, stiffness, energy dissipation, and ductility. Influence of end-plate thickness, bolt pre-tension forces, column flange slenderness and column flange stiffeners.
Plumier and Schleich [33]	4	Two external joints and two internal joints, combining bare steel columns in sections HEB300 and beams in section HEA260.	(2)	Contribution of the shear panel in the energy dissipation. Study the strength and rotation capacity of the joint.
Pradhan and Bouwkamp [31]	-	High-strength bolted joints. Beams in HEA260 and columns in HEB300. Some tests are with beam and column filled-in reinforce concrete.	-	Interactive plastification of the beam-end and column shear web panel zone, shear panel thickness and contribution of the concrete.
Bernuzzi et al. [4]	4 +	External flush and extended end plate joints, with beam IPE300 attached to a rigid counter beam.	(2)	First series studies the influence of load history. Second series studies the influence of the key geometrical and mechanical parameters in the cyclic performance.
Adey et al. [2]	8	Extended end-plate moment joints with two beam sizes W460x97 and W610x125 and one column size W310x143. End plate with 15.9 and 19.0 mm thick.	(6)	Effect of the beam size, bolt layout, end plate thickness and extension stiffeners.
Yorgun and Bayramoglu [47]	4	Bolted fabricated beam-to-column end-plate joints. (110x195) for beam and (160x135) column sizes.	(2)	Effect on cyclic load of the gap between the end plate and the column flange on the performance of the joint.
Dubina et al. [13]	2	Bolted with extended end plate beam (IPE360) to column (HEB300) internal joints	(2)	Initial stiffness, moment capacity and plastic rotation capacity.
Dubina et al. [14]	4	Bolted steel double-sided extended end-plate beam to column joints.	(2)	Evaluate the performance of the beam-to-column extended end plate, and numerical modelling of joints.
Broderick and Thomson [5]	6	Flush end-plate steel external joints. UC 203x203x86 column sizes, 254x102x22UB and 254x146x37 UB beam sizes.	(2)	Stiffness, moment capacity, rotation capacity and hysteretic behaviour.
Bursi et al. [7]	18	Bolted steel double-sided extended end-plate beam to column external joints. IPE300 beam size, HEA180, HEB180 and HEA280 column sizes.	(2)	Joint geometry and loading history.
Summer and Murray [45]	6	Bare steel double extended end-plate beam-to-column external joints. Four combinations beam/column: W24x68/W14x120, W30x99/W14/193 W36x150/W14x157, W24x68/W14x257.	(11)	Influence of the extended-end-plate in the strength, stiffness and joint ductility.
Dunai et al. [15]	19	Bolted end-plate joints with or without encased column. Columns in HEA200 or welded (6mm) changing the end plate thick, class and bolt diameters.	(2)	Study and characterise the typical cyclic behaviour failure modes of this type of joints.

Table 5. Dog Bone Beam Flange Welded Steel Joints

		Total number of research projects: 2 Total number of tests: 10 Total number of different load histories: 1		
Authors (date)	N.º of tests	Joint Characterization	Load History	Main parameters investigated
Plumier and Schleich [33]	4	Two exterior joints and two interior joints, combining bare steel columns in sections HEB300 and beams in section HEA260.	(2)	Contribution of the shear panel in the energy dissipation. Study the strength and rotation capacity joint.
Chen and Chu [9]	5+1	Five external joints with the beam (H600x300x12x20) flanges welded to the box column (500x500x20x20), and web beam bolted plates. One-storey steel frame.	-	Examine the seismic resistance characteristics of the beam-to-column assemblies.

The cyclic loads histories recorded in these tests, eleven in total, are summarized in Table 6.

Table 6. Cyclic Load Histories

Load History	N.º of tests	Description
(1)	7	Typical cyclic loading sequence which induced cyclic displacement exceeded the elastic range.
(2)	87	ECCS procedure.
(3)	3	Full reversal cycles at 0.1, 0.25, 0.50, 0.75, 1.0, 1.5, 2.0 and 3.0% interstorey drifts.
(4)	11	Based in the second-storey yield displacement ( $\delta_y$ ), three cycles were applied at each displacement of $\delta_y$ , $2\delta_y$ , $4\delta_y$ , $6\delta_y$ , etc.
(5)	10	Cyclically increasing displacements of 6 mm at the cantilever end, between each cycles.
(6)	8	Applied Technology Council Guidelines for Testing of Components of Steel Structures (ATC-24 1992).
(7)	6	Three phases of loading history: displacement increased to 5-10 mm to 15-20 mm, then decreased to the starting displacement.
(8)	32	Three cycles of 4.45 KN loops, three cycles of 8,9 KN loops, three cycles of 13.35 KN loops, two cycles of 17.8 KN loops.
(9)	15	Four different load history, defined in terms of applied beam tip displacement ( $d$ ), yield displacement $d_y$ ( $d/d_y$ ) and interstorey drift angle ( $d/H$ ) and one more load history according to the ECCS procedure.
(10)	10	5 cycles of 0.375% of drifts, 5 cycles of 0.5 %, 5 cycles of 0,75%, 3 cycles of 1%, 2 cycles of 0.5%, 2 cycles of 1.5%, 2 cycles of 0.5%, 2 cycles of 2%, 2 cycles of 0.5%, 2 cycles of 3%, 2 cycles of 0.5%, 2 cycles of 4%, 2 cycles of 0.5%, 2 cycles of 5%, 2 cycles of 0.5% and 8 cycles of 5%.
(11)	10	SAC standard and SAC near-fault loading history.

Previous work by the authors (Nogueiro et al. [30]) investigated the effect of pinching on the seismic response of steel frames and concluded that it leads to a variation of about 20% of the joint rotation, thus increasing the ductility demand on the joints to avoid failure. It is the objective of this paper: (i) to present a hysteretic model with pinching based on the Richard-Abbott mathematical model and developed by Della Corte et al. [11]; (ii) to describe the computer implementation and

adaptation of the model in a spring element within the computer code SeismoStruct (SeismoStruct [41]); (iii) to apply and calibrate the model with a series of experimental test results for steel joints subjected to cyclic loading; and (iv) to compare and propose typical parameters for the chosen joint configurations.

## 2. MODIFIED RICHARD-ABBOTT MODEL

The modified Richard-Abbott model was developed by Della Corte et al. [11], to include pinching. According to this model, the loading curve for a generic branch of the moment-rotation curve of a joint is given by the following equation:

$$M = M_n - \frac{(k_a - k_{pa}) \cdot (\phi_n - \phi)}{\left[ 1 + \left| \frac{(k_a - k_{pa}) \cdot (\phi_n - \phi)}{M_{0a}} \right|^N \right]^{1/N}} - k_{pa} \cdot (\phi_n - \phi) \quad (1)$$

where  $M_{0a} = M_n + M_{0p}$ . The unloading curve is obtained in the same way, replacing  $(M_n, \phi_n)$  by  $(M_p, \phi_p)$  and the parameters  $M_{0a}$ ,  $k_a$  and  $k_{pa}$  by the corresponding values evaluated at unloading,  $M_{0d}$ ,  $k_d$  and  $k_{pd}$ .

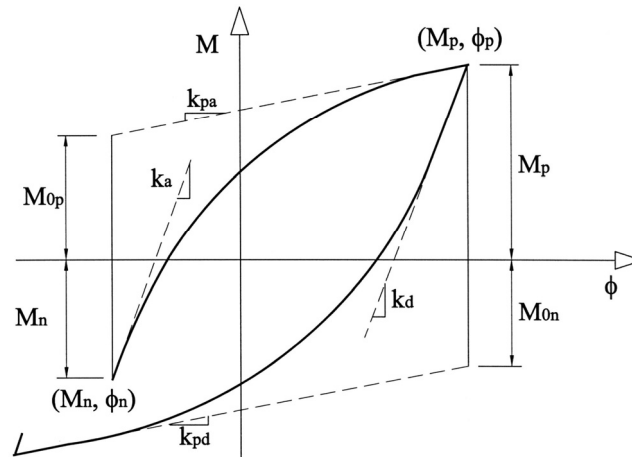


Figure 2. Generic Loading and Unloading Branches

To describe the pinching phenomenon, two limit curves are introduced, that represent a lower and an upper bounds to possible  $M$ - $\phi$  values. Both curves have a Richard-Abbott type law, and are characterised by parameters  $K_{op}$ ,  $M_{op}$ ,  $K_{hp}$ ,  $n_p$  (lower bound curve) and  $K_o$ ,  $M_o$ ,  $K_h$ ,  $n$  (upper bound curve). Additionally, any generic point  $(M, \phi)$  along the real path is also considered to belong to a Richard-Abbott type curve, where the relevant parameters are defined as follows:

$$K_{ot} = K_{op} + (K_o - K_{op}) \times t \quad (2a)$$

$$M_{ot} = M_{op} + (M_o - M_{op}) \times t \quad (2b)$$

$$K_{ht} = K_{hp} + (K_h - K_{hp}) \times t \quad (2c)$$

$$n_t = n_p + (n - n_p) \times t \quad (2d)$$

The parameter  $t$ , ranging in the interval  $[0,1]$ , defines the transition law from the lower bound to the upper bound curve. It must reproduce, as closely as possible, the shape of the experimental curves and is given by:

$$t = \left[ \frac{(\phi / \phi_{lim})^{t_1}}{(\phi / \phi_{lim})^{t_1} + 1} \right]^{t_2} \quad (3)$$

where  $t_1$ ,  $t_2$  and  $\phi_{lim}$  are three experimentally calibrated parameters. Figure 3 illustrates, qualitatively, the resulting pinching behaviour with reference to one single excursion from the origin.

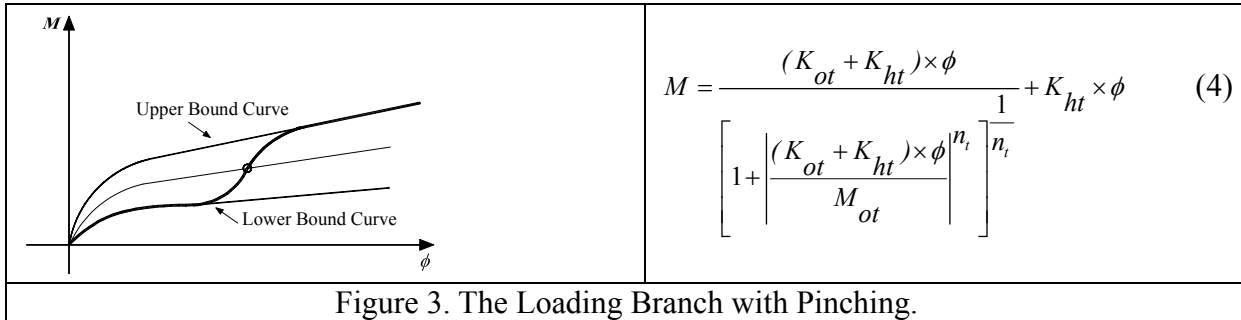


Figure 3. The Loading Branch with Pinching.

In case of a generic deformation history, the parameter  $\phi_{lim}$  is related to the maximum experienced deformation in the direction of the loading branch to be described. It is evaluated according to the following relationship:

$$\phi_{lim} = C(|\phi_o| + \phi_{max}) \quad (5)$$

where  $|\phi_o|$  is the absolute value of the deformation corresponding to the starting point of the current excursion,  $\phi_{max}$  is the maximum absolute value of the deformation experienced in the previous loading history, in the direction of loading branch to be described (Figure 4a) and  $C$  is a calibration parameter. The unloading branch is assumed to be linear with a slope equal to the initial stiffness  $K_o$  up to the interception with the straight line obtained drawing a parallel to the hardening line going through the origin. This allows the Bauschinger effect to be considered.

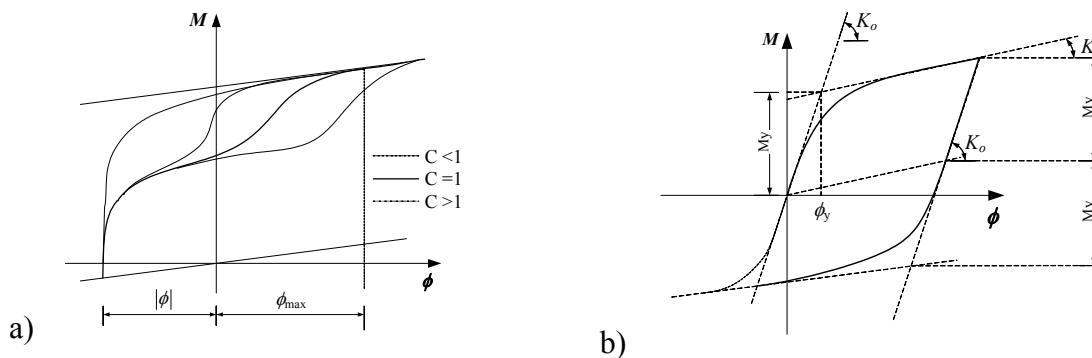


Figure 4. a) Effect of Parameter  $C$ ; b) Definition of the Unloading Branch.

Cyclic action in the inelastic range produces accumulation of plastic deformation, until ductility of the system is locally exhausted and failure occurs due to fracture. In some cases, the repetition of loading is accompanied by degradation of the structural response because of deterioration of its mechanical properties. This can be taken into consideration both for strength ( $M_{o,red}$ ) and stiffness ( $K_{o,red}$ ) using the following expressions:

$$M_{o,red} = M_o \left( 1 - i_M \times \frac{E_h}{M_y \times \phi_{u,o}} \right) \quad (6)$$

$$K_{o,red} = K_o \left( 1 - i_K \times \frac{E_h}{K_o \times \bar{\phi}_{u,o}} \right).$$

$\bar{\phi}_{u,o}$  is the corresponding ultimate value in the case of one single excursion from the origin (monotonic loading),  $E_h$  is the hysteretic energy accumulated in all previous experienced excursions,  $M_y$  represents the conventional yield resistance of the joint,  $K_o$  the initial stiffness as defined in the Figure 4b and coefficient  $i$  is an empirical parameter related to damage rate.

Hardening due to cyclic plastic deformation is considered to be isotropic. Besides, experimental results of constant deformation amplitude tests for joints not exhibiting strength deterioration show that cyclic hardening grows up in few cycles and then becomes stable. Therefore, the following assumption is made:

$$\begin{aligned} M_{o,inc} &= M_o && \text{if } \phi_{max} \leq \phi_y \\ M_{o,inc} &= M_o \left( 1 + H_h \times \frac{\phi_{max} - \phi_y}{\phi_y} \right) && \text{if } \phi_{max} \geq \phi_y \end{aligned} \quad (7)$$

$M_o$  and  $M_{o,inc}$  are the initial and increased value of strength, respectively;  $\phi_{max}$  is the maximum value of deformation reached in the loading history (in either positive or negative direction);  $\phi_y$  is the conventional yielding value of deformation (see Figure 4b);  $H_h$  is an empirical coefficient defining the level of the isotropic hardening (Filippou et al. [19]). The above formulation practically corresponds to translate the asymptotic line of the original Richard-Abbott equation (De Martino et al. [10]), as a function of the extent of the plastic deformation.

### 3. COMPUTATIONAL IMPLEMENTATION

The numerical implementation of the hysteretic model described above was carried out using the Delphi (Delphi 7 [12]) development *platform*. A six degree-of-freedom spring element was implemented in the structural analysis software SeismoStruct [41]. The implementation comprised two major parts. The first consists of the management of the hysteretic cycles, where a clear distinction between positive and negative moment must be made because of possible asymmetry of joint response under hogging or sagging bending. An illustrative flowchart of the cycle management is shown in Figure 5.

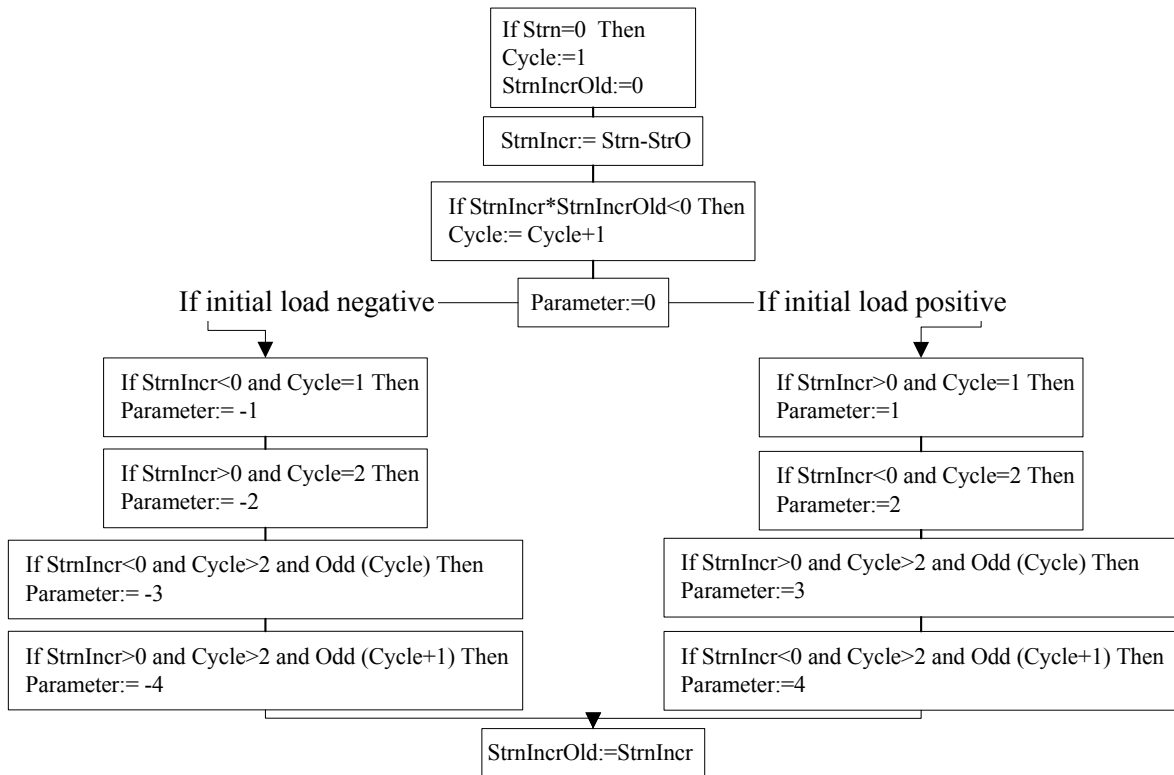


Figure 5. Flowchart for the Management of Hysteretic Cycles.

The second part of the implementation relates to the development of the code for each cycle. Several possibilities must be considered, depending on the starting bending moment (positive or negative) and the sign of the strain increment (positive or negative), as can be seen in the figure 6a, b and c.

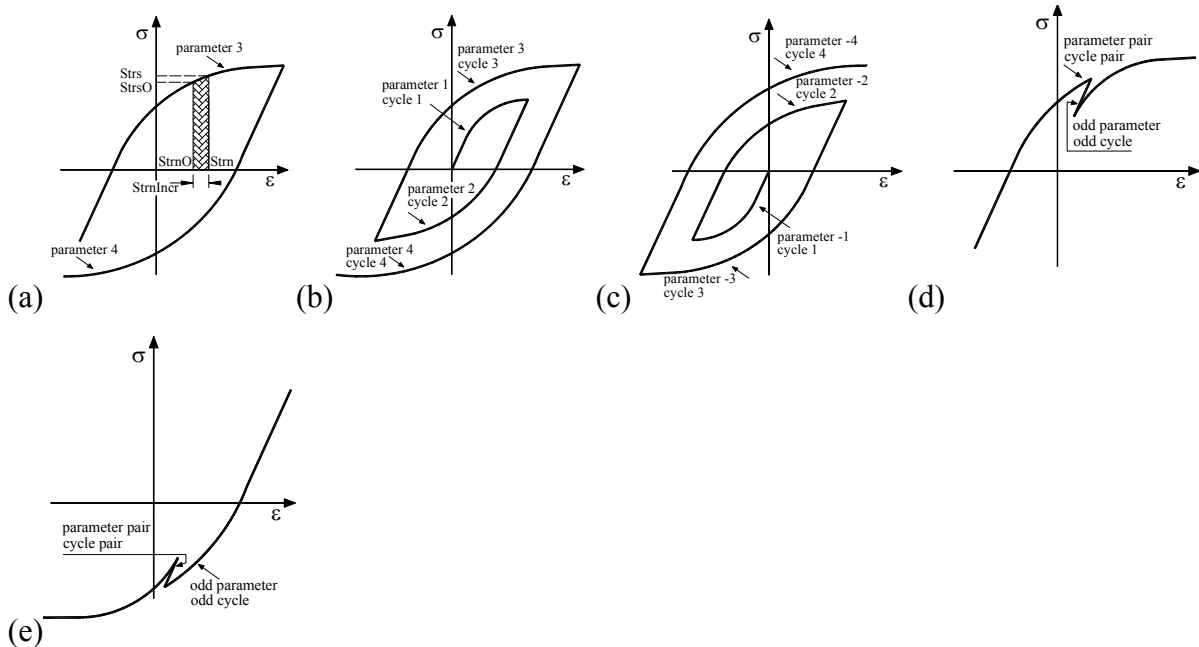


Figure 6. a) Definition of the Increment; b) Hysteretic Curve for Positive Starting; c) Hysteretic Curve for Negative Starting; d) Small Loading for Odd Parameters, e) Pair Parameters.

In total, 30 parameters have to be defined for this model, fifteen for the ascending branches (subscript  $a$ ) and fifteen for the descending branches (subscript  $d$ ):  $K_a$  (and  $K_d$ ) is the initial stiffness,  $M_a$  (and  $M_d$ ) is the moment resistance,  $K_{pa}$  (and  $K_{pd}$ ) is the post limit stiffness,  $n_a$  (and  $n_d$ ) is the shape parameter, all these for the upper bound curve (see figure 1),  $K_{ap}$  (and  $K_{dp}$ ) is the initial stiffness,  $M_{ap}$  (and  $M_{dp}$ ) is the strength,  $K_{pap}$  (and  $K_{pdp}$ ) is the post limit stiffness,  $n_{ap}$  (and  $n_{dp}$ ) is the shape parameter, all these for the lower bound curve,  $t_{1a}$  and  $t_{2a}$  (and  $t_{1d}$  and  $t_{2d}$ ) are the two parameters related to the pinching,  $C_a$  (and  $C_d$ ) is the calibration parameter related to the pinching, normally equal to 1 (see figure 4a),  $i_{Ka}$  (and  $i_{Kd}$ ) is the calibration coefficient related to the stiffness damage rate,  $i_{Ma}$  (and  $i_{Md}$ ) is the calibration coefficient related to the strength damage rate,  $H_a$  (and  $H_d$ ) is the calibration coefficient that defines the level of isotropic hardening and  $E_{maxa}$  (and  $E_{maxd}$ ) is the maximum value of deformation.

The model had to be prepared to work with any kind of loads, especially for the seismic action where loading and unloading branches can be either large or small. So, the model must be prepared to consider a reversal of loading like the one presented in Figure 6d and e, for both positive and negative starting points.

To illustrate the application and versatility of the model, it was first tested on a typical steel joint with its properties defined in Table 7, considering stiffness and strength deterioration but no hardening.

Table 7. Joint Parameters

$K_a$ KNm/rad	$M_a$ KNm	$K_{pa}$ KNm/rad	$n_a$	$K_{ap}$ KNm/rad	$M_{ap}$ KNm	$K_{pap}$ KNm/rad	$n_{ap}$	$t_{1a}$	$t_{2a}$	$C_a$	$i_{Ka}$	$i_{Ma}$	$H_a$	$E_{maxa}$ rad
34440	116	1700	2	34440	60	1700	1	10	0.15	1	15	0.01	0	0.1
$K_d$ KNm/rad	$M_d$ KNm	$K_{pd}$ KNm/rad	$n_d$	$K_{dp}$ KNm/rad	$M_{dp}$ KNm	$K_{pdp}$ KNm/rad	$n_{dp}$	$t_{1d}$	$t_{2d}$	$C_d$	$i_{Kd}$	$i_{Md}$	$H_d$	$E_{maxd}$ rad
44440	136	1700	2	44440	80	1700	1	10	0.15	1	15	0.01	0	0.1

Firstly two monotonic loadings were considered, one positive and another negative. Subsequently, two distinct cyclic load histories were applied (ECCS load history and a random load history). The results, illustrated in Figure 7, show that, for low rotations ( $< \theta_y$ ), the cyclic results coincide with the monotonic results. With increased rotation, the cyclic response deviates from the monotonic response because of strength and stiffness deterioration.

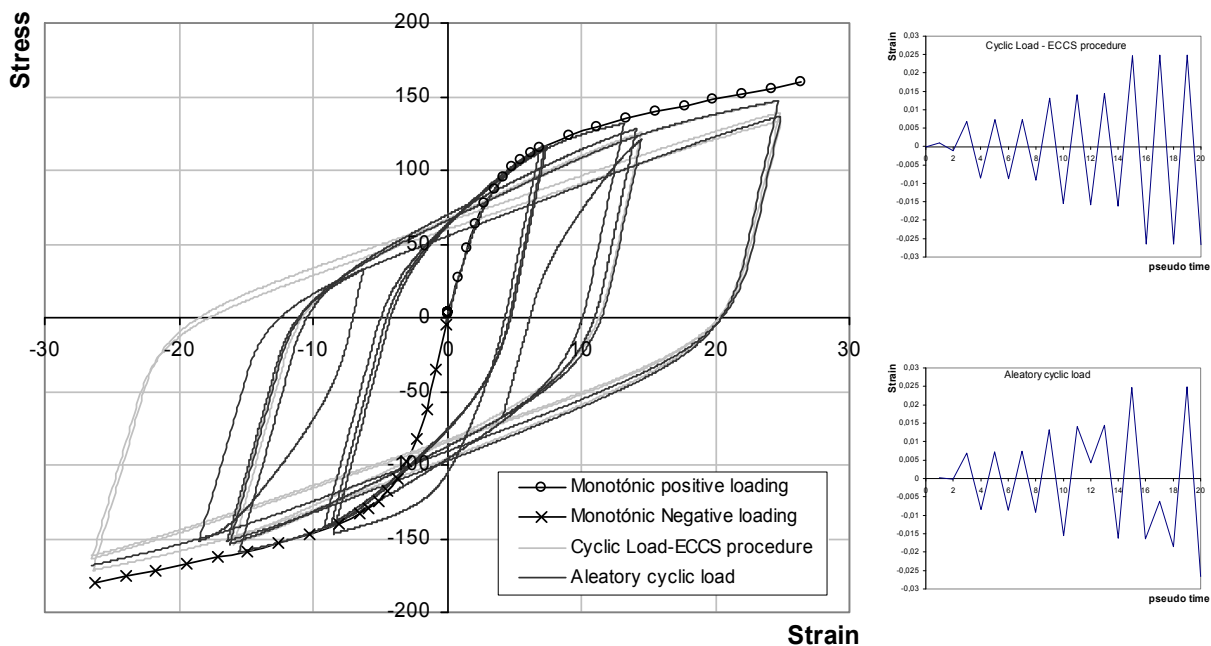


Figure 7. Hysteretic and Monotonic Curves.

## 4. APPLICATION AND VALIDATION

### 4.1 Description of the Experimental Tests

In order to establish reliable parameters for a range of end-plate or cleated beam-to-column steel joint configurations and to validate the accuracy of the model, a group of well-documented experimental results were selected from tables 1 to 8. These tests were performed by Bernuzzi *et al.* [4], Elnashai *et al.* [17], Korol *et al.* [22], Broderick *et al.* [5], Bursi *et al.* [7] and Abolmaali *et al.* [1] and are summarized in Table 8, corresponding to extended end-plate, flush end-plate, top and seat and web cleat connections.

Table 8. Experimental Tests

N°	Test Ref.	Authors	Typology	Beam	Column	Bolts	Thickness plate	$K_y^+$ KNm/rad	$K_y^-$ KNm/rad
1	EPBC-1	Bernuzzi <i>et al.</i>	Extended	IPE300	“Rigid plate”	M20	12 mm	78000	97500
2	JB1-3A	Bursi <i>et al.</i>	Extended	IPE300	HEB180	M20	18 mm	35000*	35000*
3	A2	Korol <i>et al.</i>	Extended	W360x45	W360x64	Ø 25	25.4 mm	63751	63741
4	A3	Korol <i>et al.</i>	Extended	W360x45	W360x79	Ø 25	19.0 mm	79370	79370
5	FPC/D	Bernuzzi <i>et al.</i>	Flush	IPE300	“Rigid plate”	M20	12 mm	19000	30500
6	EP4	Broderick <i>et al.</i>	Flush	254x146x37UB	203x203x86UC	M20	12 mm	3550	3550
7	EP2	Broderick <i>et al.</i>	Flush	254x102x22UB	203x203x86UC	M20	12 mm	10210	10210
8	CS01	Elnashai <i>et al.</i>	Top and Seat	254x146x31UB	203x203x6UC	Ø 16	8 mm	4300	4300
9	CS02	Elnashai <i>et al.</i>	Top and Seat	254x146x31UB	203x203x6UC	Ø 16	12 mm	7500	7500
10	CS03	Elnashai <i>et al.</i>	Top and Seat	254x146x31UB	203x203x6UC	Ø 16	15 mm	9800	9800
11	TSC/D	Bernuzzi <i>et al.</i>	Top and Seat	IPE300	“Rigid plate”	M20	12 mm	12800	20100
12	DW-WB 4	Abolmaali <i>et al.</i>	Web cleat	W410x67	W200x100	Ø 19	10 mm	32263	32263
13	DW-WB 5	Abolmaali <i>et al.</i>	Web cleat	W410x67	W200x100	Ø 19	19 mm	16254	16254

\* Estimated value

The description of the tests starts with the extended end-plate connection tests performed by Bernuzzi *et al.* [4], Bursi *et al.* [7] and Korol *et al.* [22].

The study developed by Bernuzzi *et al.* had two series of tests on beam-to-column joints under cyclic loading. The first series of tests aimed at investigating the influence of the loading history on the joint performance. The second series of tests was subsequently performed with the goal of setting the key parameters enabling a full description of the connection response, including the energy dissipation capability. From this study only three tests were chosen. The first test, referred to as EPBC-1, considers end-plates extended on both sides of the beam, as shown in Figure 8a. The plate extension ensures a noticeable increase in stiffness and strength, when compared with the others tests FPC/D and TSC/D from the same author (Table 8), later discussed. Failure occurred in the weld of the extended plate. The second test, also an end-plate extended both sides but with 18 mm plate thickness, was performed by Bursi *et al.* (Figure 8b) and results in an increase of strength; therefore the hysteretic response is quite different, as can be observed in Figure 12. Similarly, the failure mode was at weld toe, in the end plate, starting with a ductile crack at the steel surface owing to plastic strains, a stable growth of a ductile crack in the plate thickness followed by a sudden propagation of the crack in a brittle fracture mode.

Tests number 3 and 4 (Table 8), performed by Korol et al., are also extended end-plate connections, but with transverse stiffeners in the column web, as well in the end-plate, as can be seen in Figure 8c. These are stronger joints, without slippage, but much more influenced by stiffness and strength deterioration. Both exhibited failure by beam local buckling, the column flange being the first yielded component for test A2 (test number 3) and the beam web buckling for test A3 (test number 4).

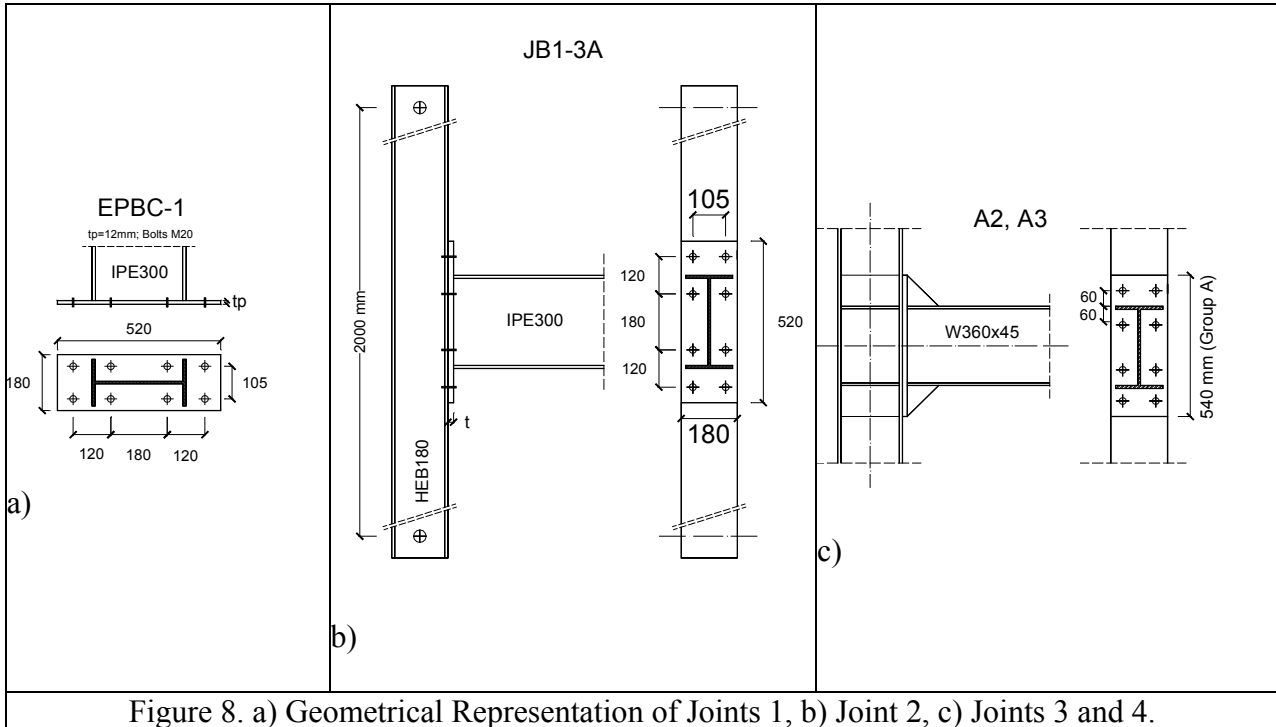


Figure 8. a) Geometrical Representation of Joints 1, b) Joint 2, c) Joints 3 and 4.

The second group of tests corresponds to flush end plate joints (test numbers 5 to 7, Table 8). The first test from this group was performed by Bernuzzi et al., and the other two by Broderick et al. The corresponding geometrical characteristics are presented in Figure 9a and 9b, respectively. In the FPC/D tests, the endplate played the most important role in the deformation, while the bolts exhibited a negligible contribution. The plastic deformation is mainly concentrated in the end plate and the failure mode was finally related to weld fracture in the internal part of the beam flange.

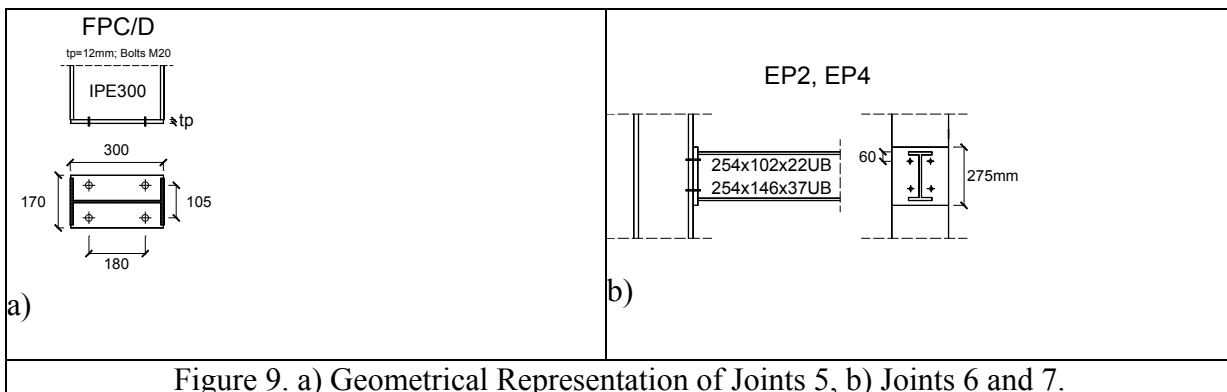


Figure 9. a) Geometrical Representation of Joints 5, b) Joints 6 and 7.

The next four tests were performed by Elghazouli et al. and Bernuzzi et al. and the geometrical representation of joints are shown in Figure 10. For the first three tests (Figure 10a), top, seat and web cleat connections, an axial load of 400 kN was applied to the column, which represents 29% of the column section plastic capacity. The CS01 joint is the most flexible and with lesser resistance and has a relatively low-energy dissipation capacity. The CS02 connection is stronger, with higher

stiffness. The CS03 has the strongest and the most stiffened connection. For all cases, the strains on the web of the connection panel zone were measured and the values were well below yield. These connections have no slippage. The TSC/D test is a top and seat connection and the failure mode is governed by the plastic deformation of the flange cleats (including hole ovalisation) and by the fracture of one bolt for large deformations, after 60 mrad, which is not recommended for seismic design.

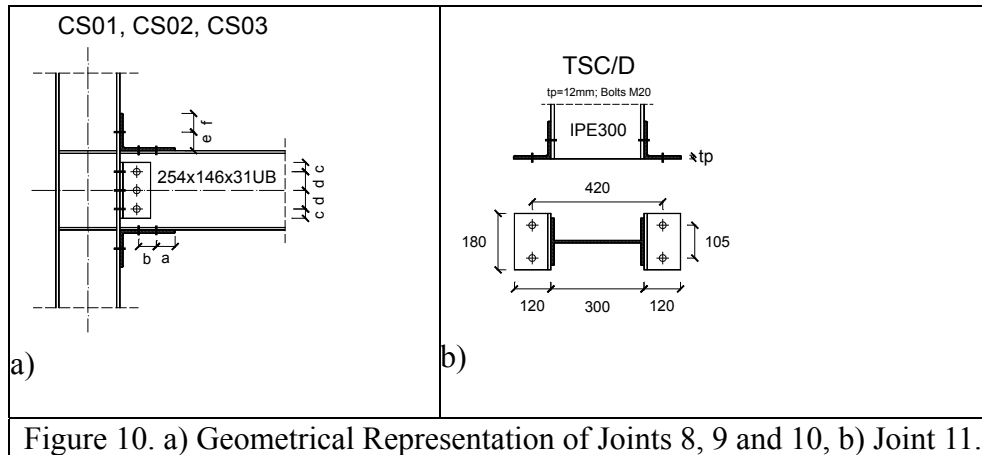


Figure 10. a) Geometrical Representation of Joints 8, 9 and 10, b) Joint 11.

Finally, the last two tests, DW-WB4 and DW-WB5, are web cleat connections (Figure 11) and were performed by Abolmaali et al.. This type of joints are very much influenced by slippage, which leads to a low rate of energy dissipated. In his study, Abolmaali et al. presented the cyclic behaviour of two series of tests corresponding to two types of semi-rigid double web cleat connections: bolted-bolted and welded-bolted (cleats welded to the beam web and bolted to the column flange), with pre-tensioned bolts, as can be seen in Figure 11. The first series of tests was rejected because of inappropriate seismic behaviour. In the second series of tests only two tests were chosen from the eight performed, respectively test DW-WB numbers 4 and 5, which exhibited yielding of the angles as the failure mode.

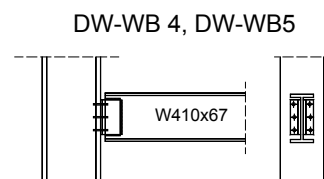


Figure 11. Geometrical Representation of Joints 12 and 13.

## 4.2 Application of the Modified Richard-Abbot model

This section presents the results of the application of the modified Richard-Abbott model to the selected tests. It is noted that almost all of the experimental curves presented in this work were rebuilt by means of the curves published in the corresponding papers, a process that can lead to some errors. The accuracy of this process dictated the selection of the tests where, whenever possible, at least one test per typology was chosen, based on the type of the mode failure.

Firstly, the figures overlaying, for each experimental hysteretic curve, the numerical curve obtained using the modified Richard-Abbott model are presented. Then, a comparison between both curves in terms of dissipated energy and moment resistance for each cycle is also presented. Finally, Tables 9 and 10 show the parameters chosen in the Richard-Abbott model, for the ascending and descending branches.

For the first two tests, with similar geometrical properties, the corresponding moment-rotation curves are shown in Figure 12. Joint number 1 has more stiffness and pinching, and has also more stiffness and strength deterioration than joint number 2. The latter has more strength, a more stable hysteretic behaviour and, as no pinching occurs, can dissipate much more energy (see also Figure 13).

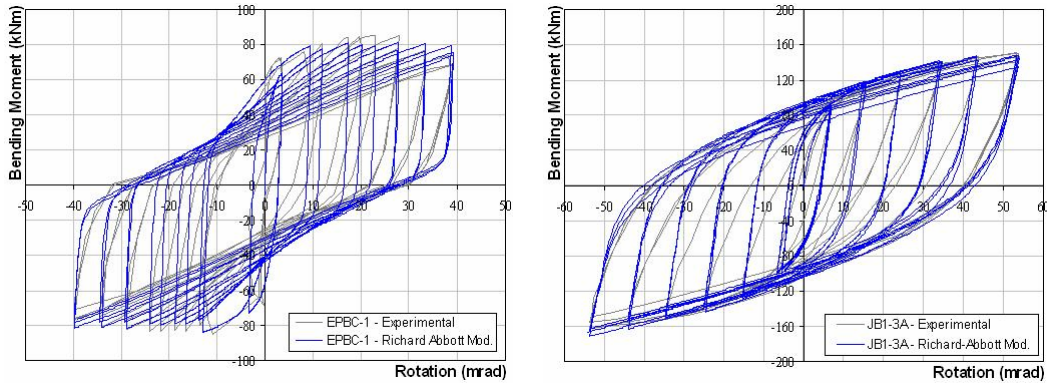


Figure 12. Hysteretic Curves for Joints 1 and 2.

To assess the accuracy of the model, the dissipated energy and the moment resistance in each cycle from the experimental tests and the Modified Richard-Abbott model were evaluated. These results are graphically presented in Figures 13 and 14. The percentage of error in each cycle was also evaluated and the results obtained are presented in all the graphs. It can be seen that, for large values of rotation, corresponding to higher values of hysteretic energy dissipation, the errors are small. Thus, in this situation, a very good agreement between the experimental and the numerical values was found.

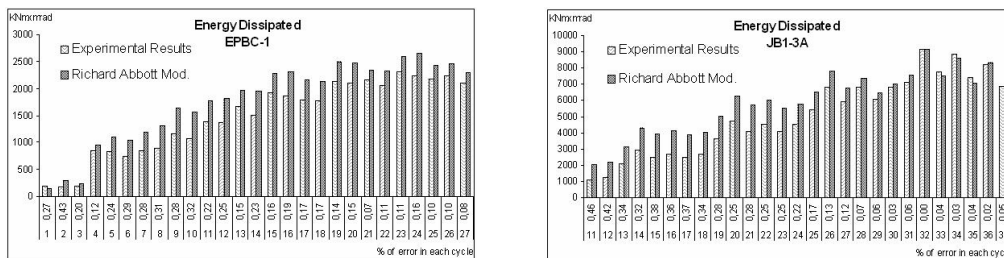


Figure 13. Energy Dissipated in Each Cycle for Joints 1 and 2.

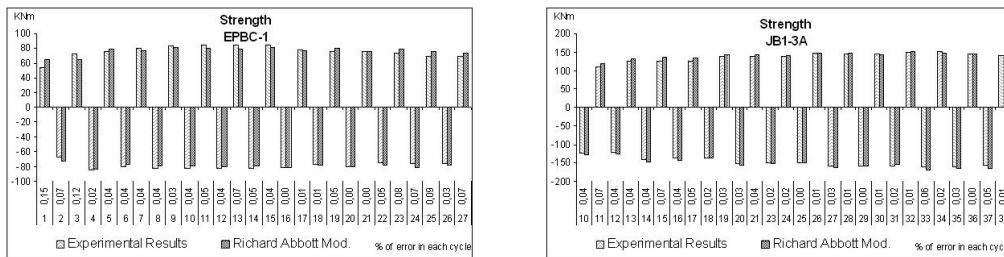


Figure 14. Moment Resistance in Each Cycle for Joints 1 and 2.

Tests number 3 and 4, with more strengthen joints than the previous tests, have no pinching, but are much more influenced by stiffness and strength deterioration, as can be seen in Figure 15. For both tests, the specimen had a good cyclic performance in terms of dissipated energy, as is shown in Figure 16. Moreover, the hysteresis loops were stable up to the onset of beam web buckling, at which beam-moment deterioration developed. The experimental and numerical curves are very close, and the model parameters are presented in Tables 9 and 10. The values of the dissipated

energy for both curves are very similar. The moment resistance values are also very similar, leading to a very small value of error, as represented in Figure 17.

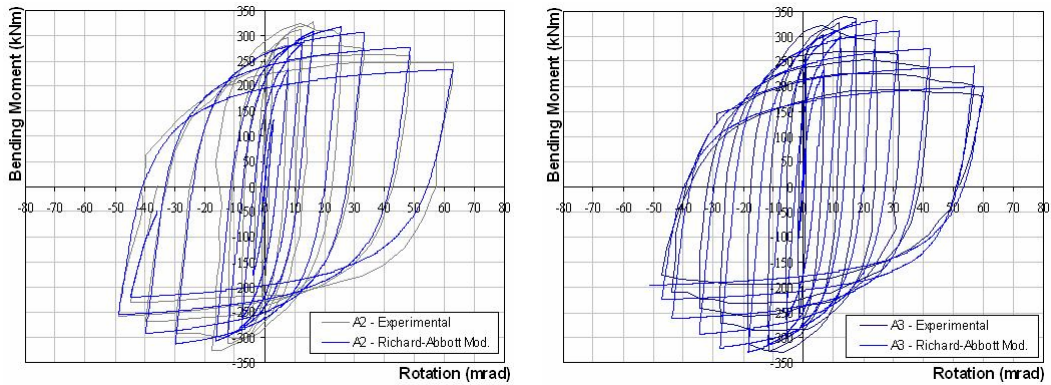


Figure 15. Hysteretic Curves for Joints 3 and 4.

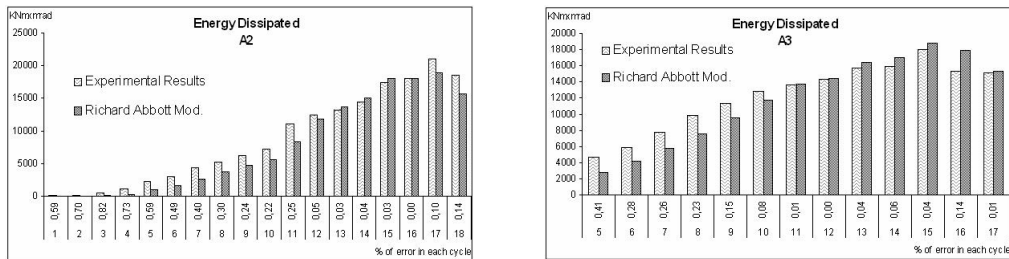


Figure 16. Energy Dissipated in Each Cycle for Joints 3 and 4.

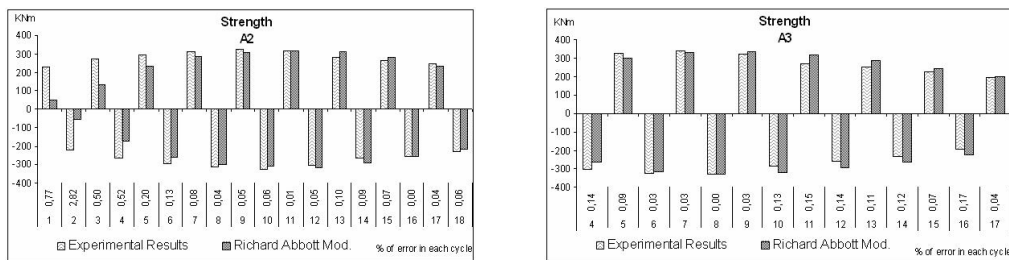


Figure 17. Moment Resistance in Each Cycle for Joints 3 and 4.

The test number 5 is a flush end plate joint directly bolted to a stiff support (no column), thus resulting in a stiffer joint, mostly governed by the endplate. The corresponding hysteretic curves can be observed in Figure 18. Because of their geometrical properties, test numbers 6 and 7 were much more influenced by pinching. Test EP4 had a mode 1 failure (according to the EC3) and the EP2 test had a mode 2 failure, governed by failure of the bolts. For both joints, no stiffness or strength degradation were observed, as can be seen in Figure 18 and from the parameters of Tables 9 and 10. Energy dissipation is also lower, as is shown in Figure 19, thus indicating inadequate seismic behaviour. The model is in good agreement with the experimental results, except for the final part of the EP2 test, because of its sudden failure.

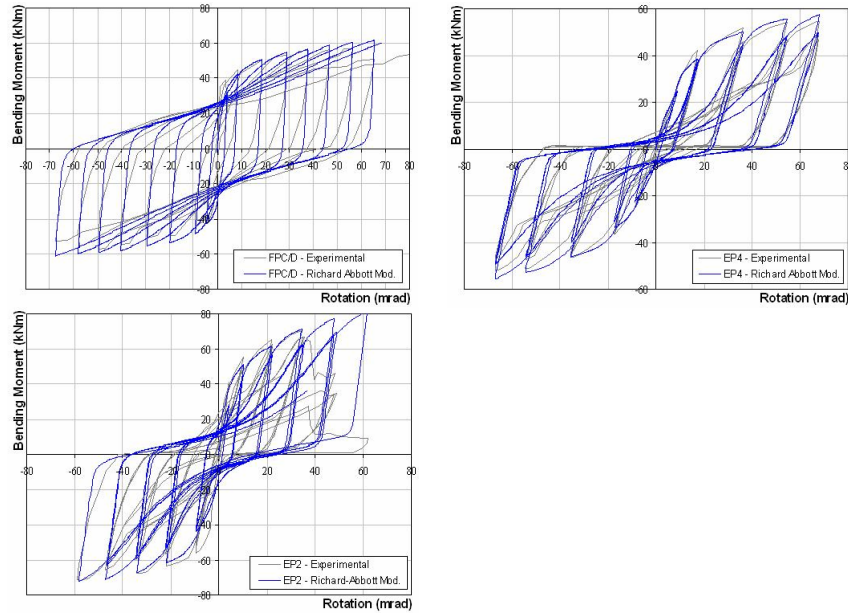


Figure 18. Hysteretic Curves for Joints 5, 6 and 7.

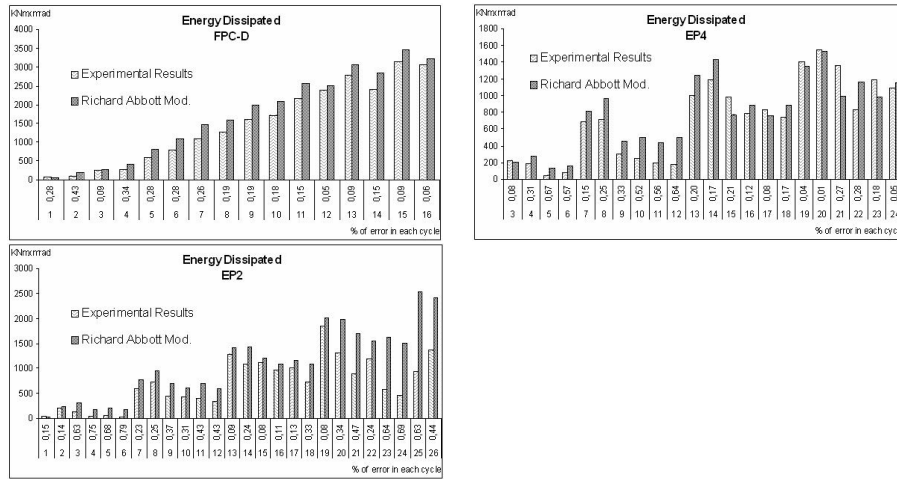


Figure 19. Energy Dissipated in Each Cycle for Joints 5, 6 and 7.

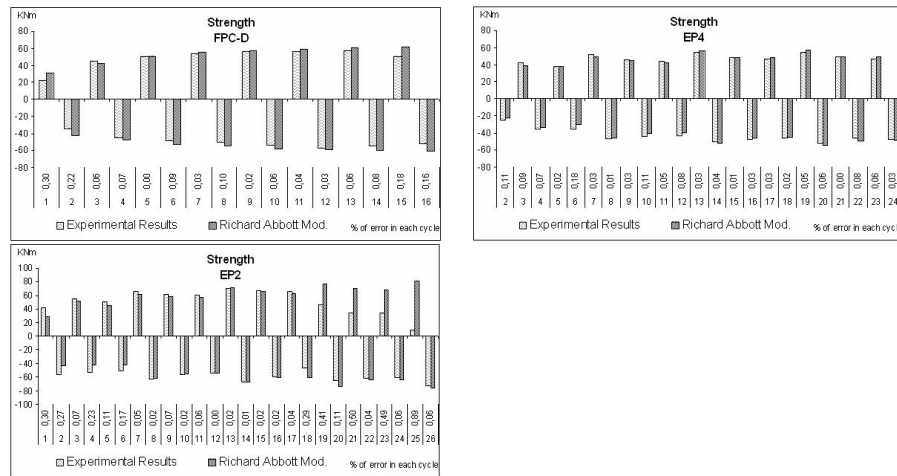


Figure 20. Moment Resistance in Each Cycle for Joints 5, 6 and 7.

The hysteretic behaviour for the top and seat cleat joints (8 to 11) is represented in Figure 21. Figures 22 and 23 depict the energy dissipation and the moment resistance, cycle by cycle. For the first test, the agreement of the experimental and numerical curves is not so good. The parameters adopted in the numerical model are also indicated in Tables 9 and 10. Joint 11 presents significant pinching, in contrast with the first three cases.

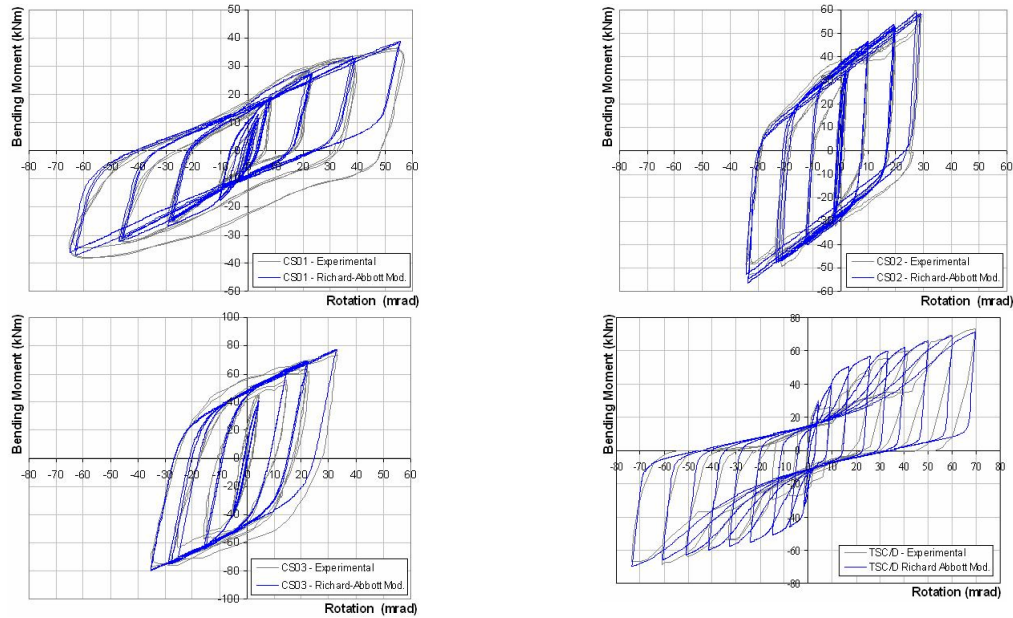


Figure 21. Hysteretic Curves for Joints 8, 9, 10 and 11.

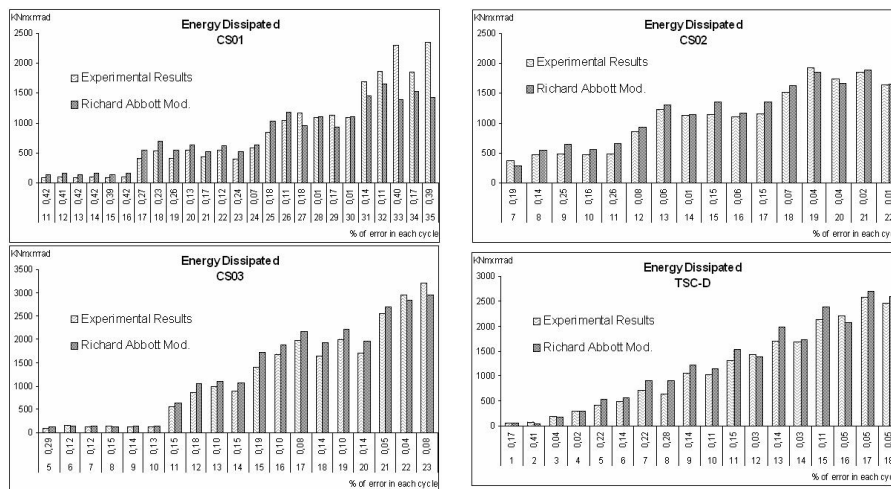


Figure 22. Energy Dissipated in Each Cycle for Joints 8, 9, 10 and 11.

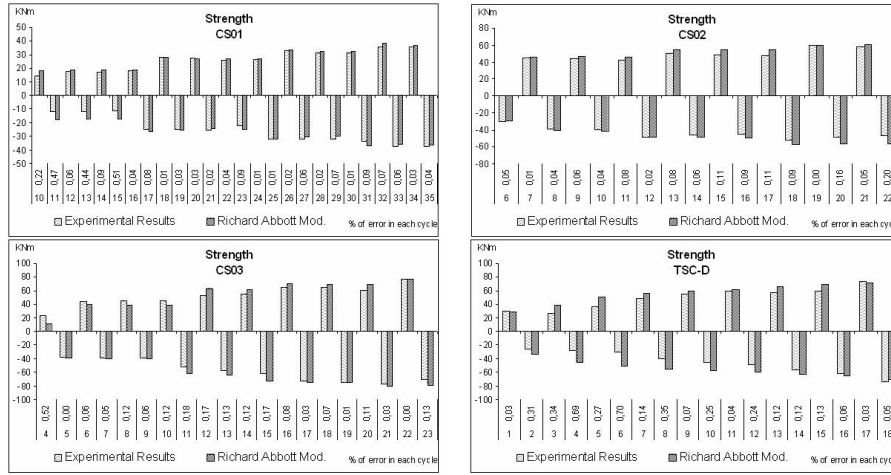


Figure 23. Moment Resistance in Each Cycle for Joints 8, 9, 10 and 11.

Finally, for the last two tests, Figure 24 compares the experimental and the numerical curves. These tests have a better hysteretic behaviour than the flush end-plate joints, more stable and with more energy dissipation capacity. A good agreement between both curves was also obtained, as it is shown in Figures 25 and 26, for dissipated energy and strength, respectively. The parameters of the numerical model are presented in Tables 9 and 10.

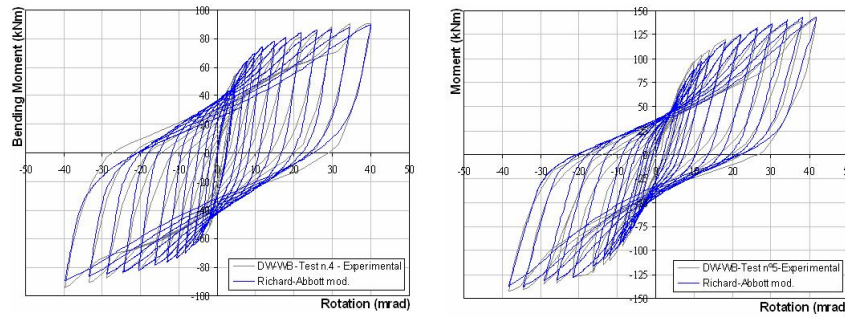


Figure 24. Hysteretic Curves for Joints 12 and 14.

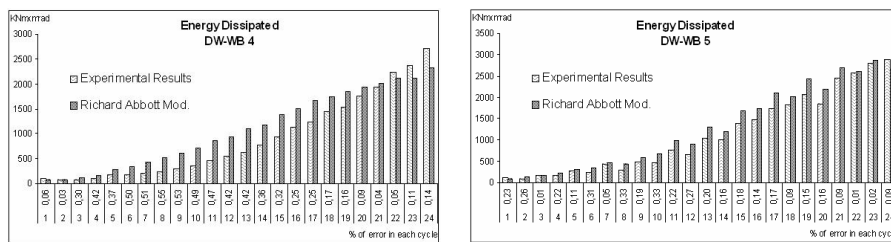


Figure 25. Energy Dissipated in Each Cycle for Joints 12 and 13.

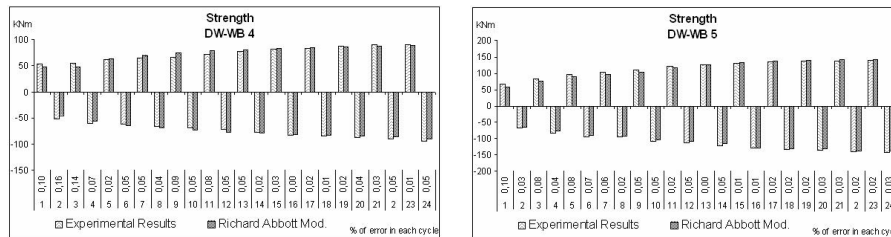


Figure 26. Moment Resistance in Each Cycle for Joints 12 and 13.



### 4.3 Discussion

Tables 9 and 10 highlight a significant dispersion of the various parameters for the different joint typologies. Some of these parameters are directly related to the static monotonic response of the joint:  $K_a$  and  $K_d$  (initial stiffness),  $M_a$  and  $M_d$  (moment resistance),  $K_{pa}$  and  $K_{pd}$  (post limit stiffness),  $n_a$  and  $n_d$  (shape parameter). They are obtainable from the direct application of the component method (Eurocode 3 [18]), as illustrated in Table 11 for the three selected flush end-plate joints.

Table 11. Monotonic Moment-rotation Parameters for the Flush End-plate Tests

Joint	Author	EC3 (COP <sup>®</sup> )		EC3 (Broderick)		Experimental		Failure Mode (T-stub)
		$K_{ini}$ KNm/rad	$M_{jrd}$ KNm	$K_{ini}$ KNm/rad	$M_{jrd}$ KNm	$K_{ini}$ KNm/rad	$M_{jrd}$ KNm	
FPC-D	Bernuzzi	19926	50.5	-	-	19000	55	Predicted – 2
EP2	Broderick	11282	49.2	11480	56.4	10210	67.7	Predicted – 2 Observed – 2
EP4	Broderick	11388	54.6	11480	49.2	3550	51.9	Predicted – 2 Observed – 1

Of greater complexity remains the establishment of the values of the remaining model parameters. Table 12 summarizes the ranges of variation for each typology.

Table 12. Variation of the Model Parameters for All Typologies

Joint Typ.	EEP		FEP	TS		WC		EEP		FEP	TS		WC
	U	S		WC	-			U	S		WC	-	
$n_a$	1	1	1	1-2	1-2	1	$n_d$	1	1	1	1-2	1	1
$K_a/K_{ap}$	1	?	1	?	?	1	$K_d/K_{dp}$	1	?	1	1-∞	1	1
$M_a/M_{ap}$	1.45-1.5	?	2-12	?	3.7	1.5-2.84	$M_d/M_{dp}$	1.6-1.625	?	2.5-10	1-∞	5	2.84
$K_{pa}/K_{pap}$	1	?	1-1.5	?	1	1	$K_{pd}/K_{pdp}$	1	?	1-1.5	1-14.3	1	1
$n_a/n_{ap}$	1	?	1	?	?	1	$n_d/n_{dp}$	1	?	1	?	1	1
$t_{1a}$	1-15	0	10-20	0	20	15	$t_{1d}$	1-10	0	10-20	0	20	15
$t_{2a}$	0.3	0	0.3	0	0.3	0.3	$t_{2d}$	0.3	0	0.3	0	0.3	0.3
$C_a$	1	0	1	0	1	1	$C_d$	1	0	1	0	1	1
$i_{Ka}$	10-60	40	0	0	30	10-30	$i_{Kd}$	10-60	30	0	0	0	10
$i_{Ma}$	0-0.02	0.03-0.05	0-0.03	0-0.04	0	0	$i_{Md}$	0-0.2	0.03-0.05	0-0.03	0-0.04	0	0
$H_a$	0-0.02	0	0	0	0	0	$H_d$	0-0.2	0	0	0	0	0

Table 13 illustrates, for each joint, the normalised values of moment resistance and initial stiffness. It is easily recognized that, apart from the two stiffened extended end-plate joints, all other joints are partial strength connections. Furthermore, the accumulated error, both in terms of total dissipated energy or average moment resistance is quite good.

Table 13. Main Properties of the Joint Behaviour

Test Number	Critical component at joint failure	Total dissipated energy error (%)	Average moment resistance error (%)	$\frac{[M_{j,rd}]_{joint}}{[M_{pl,rd}]_{beam}}$	$\frac{[K_{j,init}]_{joint}}{\left[\frac{8EI_b}{d_b}\right]_{beam}}$	$\left[\frac{N_{sd}}{N_{pl,rd}}\right]_{column}$
1	End plate in bending	17	5	0.42	0.167	0
2	End plate in bending and web column in shear	15	4	0.76	0.075	0
3	Column flange and beam local buckling	11	31	1.54	0.110	0
4		5	21	1.57	0.137	0
5	End plate in bending	14	9	0.41	0.041	0
6	End plate in bending	11	5	0.36	0.010	0
7	End plate in bending and bolt tension	23	(*) 17	0.81	0.054	0
8		7	19	0.25	0.015	0.29
9	Large distortion of the top and seat angles	5	8	0.39	0.025	0.29
10		7	21	0.53	0.033	0.29
11	Large distortion of the top and seat angles	8	22	0.53	0.027	0
12	Yielding of the angle material	18	5	0.27	0.032	0
13		11	4	0.42	0.016	0

(\*) Until cycle 17, because after that bolt failure occurred

## 5. CONCLUSIONS

This paper presents the numerical implementation of a hysteretic model able to simulate the cyclic behaviour of a generic steel joint. It is incorporated in the structural analysis software SeismoStruct (Seismosoft [41]) as a joint element, thus allowing realistic non-linear static and dynamic structural analyses. The model was applied to thirteen experimental tests from six independent sources, showing a very good agreement with the experimental results, even when using different cyclic loading strategies. Despite the small sample size, a clear trend was observed for the required model parameters for end-plate and top and seat beam-to-column joints (Table 12).

The practical application of the model naturally requires confidence in the determination of the required parameters. The experimental tests used in this paper allow to identify lower and upper limits, but no reliability estimates of the parameters. Further tests are required to reach this stage, such as the experimental programme currently being carried out at the University of Coimbra to establish the cyclic behaviour and the corresponding cyclic parameters for double-symmetric extended end-plate beam-to-column joints. Nevertheless, some statements can be made:

- i) For a double-symmetrical joint (recommended for seismic response), the 15 ascending parameters are the same as the 15 descending parameters.
- ii) The parameters that result from static monotonic behaviour ( $K_a$ ,  $M_a$ ,  $K_{pa}$ ,  $K_d$ ,  $M_d$ ,  $K_{pd}$ ) can nowadays be obtained with sufficient accuracy from the application of the component method (EC3-1-8, 2005) for the range of joint typologies addressed in this paper.
- iii) For joints without pinching and stiffness deterioration, such as an extended end-plate with stiffened column web in the tensile and compressive areas, only 6 parameters are needed. From these parameters, the first three can be obtained using the component method and the fourth is normally 1 or 2. The last one it is always the same, equal to 0.1 rad. The parameter related to the strength damage ( $i_{Ma}$ ), can be established as an average value on the basis of a sufficient number of tests.

The influence of pinching is crucial in the establishment of the model parameters. For the end-plate joints, this is clearly noticeable and it is necessary to establish whether pinching is likely to occur. In the near future, a pragmatic way is to choose standardised steel joints, with stable hysteretic behaviour. For this case, good levels of confidence can be assumed for the choice of the model parameters. Finally, parametric studies should be carried out to assess the sensitivity of the joint response to the choice of parameters.

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